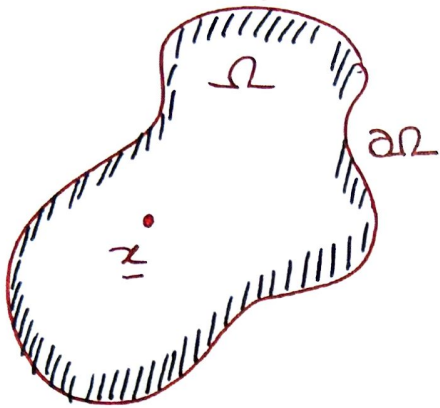


# Problem Set # 5

Q1 :



This is a standard derivation of the heat eqn for a homogeneous, continuous, isotropic solid.

By energy conservation applied to  $\Omega$ :

$$\underbrace{\frac{d}{dt} \iiint_{\Omega} \rho c T \cdot dV}_{\textcircled{1}} = - \underbrace{\iint_{\partial\Omega} \mathbf{q} \cdot \hat{\mathbf{n}} \, dS}_{\textcircled{2}}$$

The LHS  $\textcircled{1}$  is the change in total internal heat since the heat energy at a point is given by

$$E = \rho c T \leftarrow \text{temperature.}$$

↑  
density

↑  
specific heat  
or heat per unit mass

The RHS  $\textcircled{2}$  is the amount of heat leaving the boundary,  $\partial\Omega$ , where  $\mathbf{q}$  is the flux vector.

Thus  $(\mathbf{q} \cdot \hat{\mathbf{n}}) \, dS$  gives the heat leaving  $dS$ .

\* note  $(\underline{q} \cdot \underline{\hat{n}} \cdot dS) > 0$  means heat is leaving  
 so  $\iiint \rho c T \, dV$  should decrease, hence the  
 negative sign.

By Fourier's Law:  $\underline{q} = -k \nabla T$

$$\therefore \iiint_{\Omega} \frac{\partial T}{\partial t} \, dV = + \iint_{\partial \Omega} k \nabla T \cdot \underline{\hat{n}} \, dS$$

By the divergence thm,

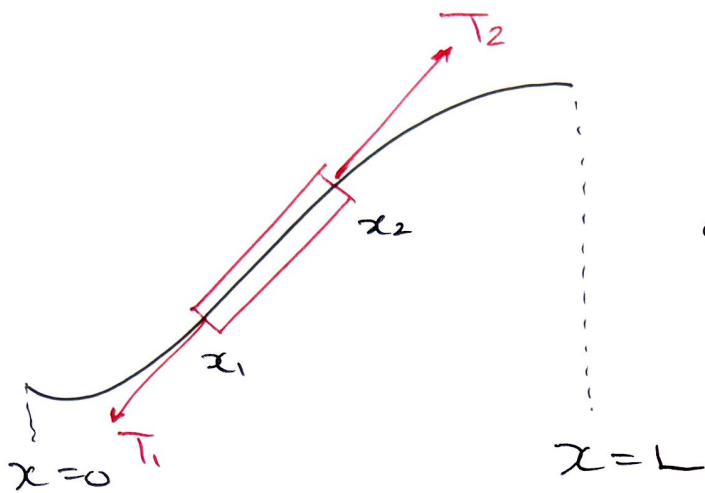
$$\begin{aligned} k \iint_{\partial \Omega} (\nabla T) \cdot \underline{\hat{n}} \, dS &= k \iiint_{\partial \Omega} \nabla \cdot (\nabla T) \, dV \\ &= k \iiint_{\Omega} \nabla^2 T \, dV \end{aligned}$$

Since this is true for the integral\*, we claim  
 it is true for the integrand

$$\frac{\partial T}{\partial t} = k \nabla^2 T.$$

\* The reason why is that we could have used any  
 subset  $\Omega^* \subseteq \Omega$  and the demonstration would  
 still be true.

# DERIVATION OF WAVE EQUATION.



## Assumptions:

- String tension is  $T$
- String density is  $\rho$
- Gravity and air resistance ignored.

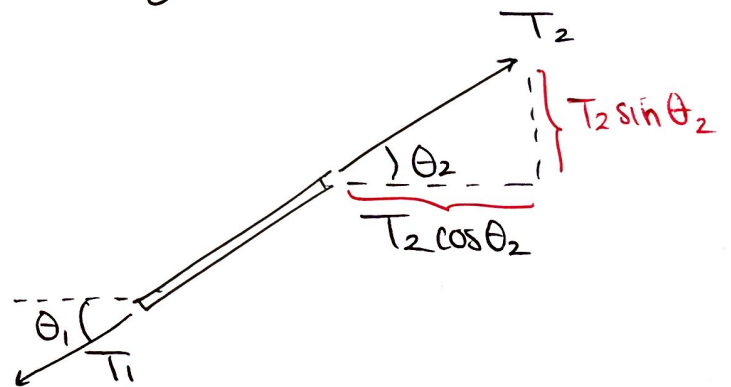
• We also assume small deflection  $\Rightarrow \left| \frac{\partial y}{\partial x} \right|$  is small.

• Consider Newton's Laws on a segment  $[x_1, x_2]$

Horizontal forces balance like

$$T_2 \cos \theta_2 = T_1 \cos \theta_1 \quad (1)$$

Vertical forces balance like



$$(\rho \Delta x) \frac{\partial^2 y}{\partial t^2}(x_0, t) = T_2 \sin \theta_2 - T_1 \sin \theta_1 \quad (2) \text{ where } x_0 \in [x_1, x_2].$$

we should use  $\Delta s = \sqrt{\Delta x^2 + \Delta y^2} = \Delta x \sqrt{1 + (\Delta y / \Delta x)^2} \sim \Delta x$  since  $\Delta y / \Delta x$  small.

• Since  $|y_x|$  small  $T_2 \cos \theta_2 \sim T_2$  and  $T_1 \cos \theta_1 \sim T_1$  since  $\theta_2$  and  $\theta_1$  are small. From (1)

$$\therefore T_2 \sim T_1$$

• Now  $\sin \theta \sim \tan \theta$  if  $\theta$  is small (since  $\cos \theta \sim 1$ )

$$\sim \frac{\partial y}{\partial x}$$

$$\therefore \sin \theta_1 \sim \frac{\partial y}{\partial x}(x_1, t) \text{ and } \sin \theta_2 \sim \frac{\partial y}{\partial x}(x_2, t)$$

Thus (2)  $\Rightarrow \rho \Delta x \frac{\partial^2 y}{\partial t^2}(x_0, t) \sim T \frac{\partial y}{\partial x}(x_2, t) - \frac{\partial y}{\partial x}(x_1, t)$

Use  $x_2 = x_1 + \Delta x \Rightarrow y_{tt}(x_0, t) \sim \frac{T}{\rho} \frac{\partial^2 y}{\partial x^2}(a, t)$

where  $a \in [x_1, x_2]$  by the MVT. Thus

$$y_{tt}(x, t) = \frac{T}{\rho} y_{xx}(x, t)$$

once we take  $\Delta x \rightarrow 0$ .

#3. (a)  $u(0, t) = T_0$  means fix the temperature  
 $u(L, t) = T_1$  at  $x=0, L$ .

$\frac{\partial u}{\partial x}(0, t) = F_0$  means fix the heat

$\frac{\partial u}{\partial x}(L, t) = F_1$  flux @  $x=0, L$

(Recall  $q = -k \frac{\partial T}{\partial x}$  so we  
are fixing the rate that  
heat is pumped in/out)

(b) Thermal insulation means that we do not  
allow heat flow  $\Rightarrow q = -k \frac{\partial T}{\partial x} = 0$ .

\* note this is not the same as saying the  
boundary is fixed at a temperature.

(c) Fixed temperature  $\Rightarrow T(\underline{x}, t) = G(\underline{x}, t)$  for  
all  $\underline{x} \in S$ . In the case the temperature is fixed  
for all time,  $T(\underline{x}, t) = b(\underline{x})$  for  $\underline{x} \in S$ .

Fixed flux  $\Rightarrow \underline{q} \cdot \underline{\hat{n}} = H(\underline{x}, t)$  or  $\nabla T \cdot \underline{n} = H(\underline{x}, t)$

Thermal insulation  $\Rightarrow \nabla T \cdot \underline{n} = 0$ .

Q4 :

$$\begin{cases} y_{tt} = c^2 y_{xx} \\ y(0, t) = 0 = y(L, t), \quad t > 0. \end{cases}$$

Assume  $y(x, t) = X(x) \cdot T(t)$

$$\Rightarrow T'' X = c^2 X'' T$$

$$\Rightarrow \frac{T''}{c^2 T} = \frac{X''}{X}$$

Since LHS is only dep. on time and RHS only dependent on  $x$ , we must have

$$\frac{T''}{c^2 T} = \frac{X''}{X} = -\lambda^2 < 0 \quad (+)$$

The constant chosen to obtain non-trivial sol'ns.

Then

$$X = A \cos(\lambda x) + B \sin(\lambda x)$$

$$T = C \cos(\lambda c t) + D \sin(\lambda c t).$$

BCs :

$$y(0, t) = 0 \Rightarrow X(0) T(t) = 0 \Rightarrow X(0) = 0$$

$$y(L, t) = 0 \Rightarrow X(L) T(t) = 0 \Rightarrow X(L) = 0$$

So we must have  $A = 0$  and

$$B \sin(\lambda L) = 0 \Rightarrow \lambda L = n\pi, \quad n \in \mathbb{Z}$$

For different  $n$  we should choose

$$y_n(x, t) = B_n \sin\left(\frac{n\pi x}{L}\right) \left\{ C_n \cos\left(\frac{n\pi ct}{L}\right) + D_n \sin\left(\frac{n\pi ct}{L}\right) \right\}$$

The  $n$  should be  $-3, -2, -1, 0, 1, 2, 3, \dots \in \mathbb{Z}$ .

But negative  $n$  can be absorbed into the coeffs

while  $n=0$  is  $y_n = 0$ .

What happens if  $\lambda^2 = 0$  in (†)?

Then  $T'' = 0 \Rightarrow T = At + B$ . To keep solutions from growing  $t \rightarrow \infty$  need  $A = 0$ .

Similarly  $X'' = 0 \Rightarrow X = Cx + D$ .

But  $X(0) = 0 = X(L) \Rightarrow C = D = 0$ .

Can verify trivial solutions for " $-\lambda^2$ "  $> 0$ . So we conclude

$$y = \sum_{n=0}^{\infty} \sin\left(\frac{n\pi x}{L}\right) \left\{ \hat{C}_n \cos\left(\frac{n\pi ct}{L}\right) + \hat{D}_n \sin\left(\frac{n\pi ct}{L}\right) \right\}$$

where  $\hat{C}_n = B_n C_n$ ,  $\hat{D}_n = B_n D_n$ .

next chapter we try to understand these functions.